

OpenGeoSys 6: Implementation of the Unsaturated Component Transport Process

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1 Unsaturated Component Transport Process

Used literature: [1] [3] [4] [2] [5] [7] [8] [6]

1.1 General Balance Equations

Let Ω be a domain, Γ the boundary of the domain and let u be an intrinsic quantity (for instance mass or heat) and the volume density is described by a function $S(u)$. The amount of the quantity in the domain can vary within time by two reasons. Firstly, new quantity can accumulate by flow over Γ or secondly it can be generated due to the presence of sources or sinks within Ω . Consequently, the balance reads

$$\frac{\partial}{\partial t} \int_{\Omega} S(u(x, t)) dx = - \int_{\Gamma} \langle J(x, t) | n(x) \rangle d\sigma + \int_{\Omega} Q(x, t) dx, \quad (1.1)$$

where $J(x, t)$ is the flow over the boundary, n is normal vector pointing outside of Ω , $d\sigma$ is an infinitesimal small surface element and $Q(x, t)$ describes sources and sinks within Ω . Further mathematical manipulations leads to

$$\int_{\Omega} \frac{\partial S(u(x, t))}{\partial t} dx + \int_{\Gamma} \langle J(x, t) | n(x) \rangle d\sigma - \int_{\Omega} Q(x, t) dx = 0. \quad (1.2)$$

Applying the theorem of Gauss yields to

$$\int_{\Omega} \frac{\partial S(u(x, t))}{\partial t} dx + \int_{\Omega} \operatorname{div} J(x, t) dx - \int_{\Omega} Q(x, t) dx = 0. \quad (1.3)$$

Finally,

$$\int_{\Omega} \left[\frac{\partial S(u(x, t))}{\partial t} + \operatorname{div} J(x, t) - Q(x, t) \right] dx = 0. \quad (1.4)$$

Since the domain is arbitrary it holds:

$$\frac{\partial S(u(x, t))}{\partial t} + \operatorname{div} J(x, t) - Q(x, t) = 0. \quad (1.5)$$

Depending on the constitutive law that describes the flow J , we obtain the balance equation of the considered process. Important practical laws are

$$J^{(1)} = -\mathbf{K} \operatorname{grad} u = -\mathbf{K} \nabla u \quad (1.6)$$

which describes diffusive flow and

$$J^{(2)} = cu \quad (\text{where } c \text{ is a velocity vector}) \quad (1.7)$$

which describes advective flow or a combination of (1.6) and (1.7). For instance, substituting (1.6) in (1.5) leads to the following parabolic partial differential equation:

$$\frac{\partial S(u(x, t))}{\partial t} - \nabla \cdot [\mathbf{K}(x, t) \nabla u(x, t)] - Q(x, t) = 0, \quad (1.8)$$

while the description of the flow by a combination of (1.6) and (1.7) yields to

$$\frac{\partial S(u(x, t))}{\partial t} - \nabla \cdot [\mathbf{K}(x, t) \nabla u(x, t) - cu(x, t)] - Q(x, t) = 0. \quad (1.9)$$

1.2 Unsaturated Flow - The Richards Equation

todo

- explain
 - porous medium,
 - saturated / unsaturated
 - wet and gas phase,
- mention all assumptions

Literature: [6, chapter 6], [2, chapter 6]

$$0 = \frac{\partial \phi \rho_w S}{\partial t} - \nabla \cdot \left(\rho_w \frac{k_{\text{rel}} \boldsymbol{\kappa}}{\mu_w} (\nabla p_w + \rho_w g e_z) \right) - Q_w \quad (1.10)$$

$$= \frac{\partial \phi}{\partial t} \rho_w S + \phi \frac{\partial \rho_w}{\partial t} S + \phi \rho_w \frac{\partial S}{\partial t} - \nabla \cdot \left(\rho_w \frac{k_{\text{rel}} \boldsymbol{\kappa}}{\mu_w} (\nabla p + \rho_w g e_z) \right) - Q_w \quad (1.11)$$

Under the assumptions

- that the porosity is constant (i.e., the first term vanishes),
- and that the pressure of the gas phase is zero, that allows for $p_c = -p$

the above equation takes the following form

$$0 = \phi \frac{\partial \rho_w}{\partial p} \frac{\partial p}{\partial t} S - \phi \rho_w \frac{\partial S}{\partial p_c} \frac{\partial p_c}{\partial t} - \nabla \cdot \left(\rho_w \frac{k_{\text{rel}} \boldsymbol{\kappa}}{\mu_w} (\nabla p_w + \rho_w g e_z) \right) - Q_w \quad (1.12)$$

where

$$p_c = \frac{\rho_w g}{\alpha} \left[S_{\text{eff}}^{-\frac{1}{m}} - 1 \right]^{\frac{1}{n}} \quad (1.13)$$

is the capillary pressure and

$$S_{\text{eff}} = \frac{S - S_r}{S_{\text{max}} - S_r} \quad (1.14)$$

is the effective saturation.

1.2.1 Boundary Conditions

$$p_w - g_D^{p_w} = 0 \quad \text{on} \quad \Gamma_D \quad (\text{Dirichlet type boundary conditions}) \quad (1.15)$$

$$\rho_w \frac{k_{\text{rel}} \boldsymbol{\kappa}}{\mu_w} \nabla^T p_w \cdot \boldsymbol{n} + g_N^{p_w} = 0 \quad \text{on} \quad \Gamma_N \quad (\text{Neumann type boundary conditions}) \quad (1.16)$$

1.2.2 Evaluating Dominance of Effects

Substitution of variables from the first term of (1.12) results in

$$\begin{aligned} \phi \frac{\partial \rho_w}{\partial p} \frac{\partial p}{\partial t} S &= \phi_c \left(\frac{\partial p}{\partial t} \right)_c \left(\frac{\partial \rho_w}{\partial p} \right)_c S_c \phi^* \left(\frac{\partial \rho_w}{\partial p} \right)^* \left(\frac{\partial p}{\partial t} \right)^* S^* = \phi_c \frac{\Delta(\rho_w)_c}{(\Delta t)_c} S_c \phi^* \left(\frac{\partial \rho_w}{\partial p} \right)^* \left(\frac{\partial p}{\partial t} \right)^* S^* \\ &= \phi_c \frac{\Delta(\rho_w)_c}{t_c} S_c \phi^* \left(\frac{\partial \rho_w}{\partial p} \right)^* \left(\frac{\partial p}{\partial t} \right)^* S^* \end{aligned} \quad (1.17)$$

see 7.7 in
[2]

The second term of (1.12) yields

$$\begin{aligned}
\phi \rho_w \frac{\partial S}{\partial p_c} \frac{\partial p_c}{\partial t} &= \phi^* \phi_c \rho_w^* (\rho_w)_c \left(\frac{\partial S}{\partial p_c} \frac{\partial p_c}{\partial t} \right)_c^* \left(\frac{\partial S}{\partial p_c} \frac{\partial p_c}{\partial t} \right)_c = \phi_c (\rho_w)_c \left(\frac{\partial S}{\partial p_c} \frac{\partial p_c}{\partial t} \right)_c \phi^* \rho_w^* \left(\frac{\partial S}{\partial p_c} \frac{\partial p_c}{\partial t} \right)_c^* \\
&= \phi_c (\rho_w)_c \frac{(\Delta S)_c}{(\Delta t)_c} \phi^* \rho_w^* \left(\frac{\partial S}{\partial p_c} \frac{\partial p_c}{\partial t} \right)_c^* = \phi_c (\rho_w)_c \frac{(\Delta S)_c}{t_c} \phi^* \rho_w^* \left(\frac{\partial S}{\partial p_c} \frac{\partial p_c}{\partial t} \right)_c^*
\end{aligned} \tag{1.18}$$

$$\begin{aligned}
\nabla \cdot \left(\rho_w \frac{k_{\text{rel}} \boldsymbol{\kappa}}{\mu_w} (\nabla p_w + \rho_w g e_z) \right) &= \frac{\partial}{\partial x_i} \cdot \left(\rho_w \frac{k_{\text{rel}} \boldsymbol{\kappa}}{\mu_w} \left(\frac{\partial}{\partial x_i} p_w + \rho_w g e_z \right) \right) \\
&= \frac{(\rho_w)_c}{L_c} \frac{(k_{\text{rel}})_c \boldsymbol{\kappa}_c}{(\mu_w)_c} \left(\frac{(\Delta p_w)_c}{L_c} + (\rho_w)_c g e_z \right) \frac{\partial}{\partial x_i^*} \left(\rho_w^* \frac{k_{\text{rel}}^* \boldsymbol{\kappa}^*}{\mu_w^*} \left(\frac{\partial p_w^*}{\partial x_i^*} + \rho_w^* g e_z \right) \right)
\end{aligned} \tag{1.19}$$

$$\begin{aligned}
0 &= \phi_c \frac{\Delta(\rho_w)_c}{t_c} S_c \phi^* \left(\frac{\partial \rho_w}{\partial p} \right)^* \left(\frac{\partial p}{\partial t} \right)^* S^* - \phi_c (\rho_w)_c \frac{(\Delta S)_c}{t_c} \phi^* \rho_w^* \left(\frac{\partial S}{\partial p_c} \frac{\partial p_c}{\partial t} \right)_c^* \\
&\quad - \frac{(\rho_w)_c}{L_c} \frac{(k_{\text{rel}})_c \boldsymbol{\kappa}_c}{(\mu_w)_c} \left(\frac{(\Delta p_w)_c}{L_c} + (\rho_w)_c g e_z \right) \frac{\partial}{\partial x_i^*} \left(\rho_w^* \frac{k_{\text{rel}}^* \boldsymbol{\kappa}^*}{\mu_w^*} \left(\frac{\partial p_w^*}{\partial x_i^*} + \rho_w^* g e_z \right) \right) \\
&= \phi_c \frac{\Delta(\rho_w)_c}{t_c} S_c \phi^* \left(\frac{\partial \rho_w}{\partial p} \right)^* \left(\frac{\partial p}{\partial t} \right)^* S^* - \phi_c (\rho_w)_c \frac{(\Delta S)_c}{t_c} \phi^* \rho_w^* \left(\frac{\partial S}{\partial p_c} \frac{\partial p_c}{\partial t} \right)_c^* \\
&\quad - \frac{(\rho_w)_c}{L_c^2} \frac{(k_{\text{rel}})_c \boldsymbol{\kappa}_c}{(\mu_w)_c} \left((\Delta p_w)_c + L_c (\rho_w)_c g e_z \right) \frac{\partial}{\partial x_i^*} \left(\rho_w^* \frac{k_{\text{rel}}^* \boldsymbol{\kappa}^*}{\mu_w^*} \left(\frac{\partial p_w^*}{\partial x_i^*} + \rho_w^* g e_z \right) \right)
\end{aligned} \tag{1.20}$$

1.2.3 Weak Formulation

Multiplying (1.12) and (1.16) with test functions $v_p, \bar{v}_p \in H_0^1(\Omega)$, integration over Ω, Γ_N and adding the results leads to

$$\begin{aligned}
0 &= \int_{\Omega} v_p \cdot \phi \frac{\partial \rho_w}{\partial p} \frac{\partial p}{\partial t} S dx - \int_{\Omega} v_p \cdot \phi \rho_w \frac{\partial S}{\partial p_c} \frac{\partial p_c}{\partial t} dx \\
&\quad - \int_{\Omega} v_p \cdot \nabla \cdot \rho_w \frac{k_{\text{rel}} \boldsymbol{\kappa}}{\mu_w} \nabla p_w dx \\
&\quad - \int_{\Omega} v_p \cdot \nabla \cdot \rho_w \frac{k_{\text{rel}} \boldsymbol{\kappa}}{\mu_w} \rho_w g e_z dx - \int_{\Omega} v_p \cdot Q_w dx + \int_{\Gamma_N} \bar{v}_p \cdot \left[\rho_w \frac{k_{\text{rel}} \boldsymbol{\kappa}}{\mu_w} \nabla^T p_w \cdot n + g_N^{p_w} \right] d\sigma.
\end{aligned} \tag{1.21}$$

Partial integration of the third integral of (1.21) leads to

$$\int_{\Omega} v_p \cdot \nabla \cdot \rho_w \frac{k_{\text{rel}} \boldsymbol{\kappa}}{\mu_w} \nabla p_w dx = \int_{\Omega} \nabla \cdot \left[v_p \cdot \rho_w \frac{k_{\text{rel}} \boldsymbol{\kappa}}{\mu_w} \nabla p_w \right] dx - \int_{\Omega} \nabla^T v_p \cdot \rho_w \frac{k_{\text{rel}} \boldsymbol{\kappa}}{\mu_w} \nabla p_w dx \tag{1.22}$$

The application of the theorem of Gauss to the first integral of the right hand side of (1.22) leads to

$$\begin{aligned}
\int_{\Omega} \nabla \cdot \left[v_p \cdot \rho_w \frac{k_{\text{rel}} \boldsymbol{\kappa}}{\mu_w} \nabla p_w \right] dx &= \int_{\Gamma} v_p \cdot \rho_w \frac{k_{\text{rel}} \boldsymbol{\kappa}}{\mu_w} \nabla p_w \cdot n d\sigma \\
&= \underbrace{\int_{\Gamma_D} v_p \cdot \rho_w \frac{k_{\text{rel}} \boldsymbol{\kappa}}{\mu_w} \nabla^T p_w \cdot n d\sigma}_{=0, \text{ since } v_p \in H_0^1(\Omega)} + \int_{\Gamma_N} v_p \cdot \rho_w \frac{k_{\text{rel}} \boldsymbol{\kappa}}{\mu_w} \nabla^T p_w \cdot n d\sigma
\end{aligned} \tag{1.23}$$

Substituting (1.23) in (1.22) and substituting the result in (1.21) yields

$$\begin{aligned}
0 = & \int_{\Omega} v_p \cdot \phi \frac{\partial \rho_w}{\partial p} \frac{\partial p}{\partial t} S dx - \int_{\Omega} v_p \cdot \phi \rho_w \frac{\partial S}{\partial p_c} \frac{\partial p_c}{\partial t} dx \\
& - \int_{\Gamma_N} v_p \cdot \rho_w \frac{k_{\text{rel}} \boldsymbol{\kappa}}{\mu_w} \nabla^T p_w \cdot \mathbf{n} d\sigma + \int_{\Omega} \nabla^T v_p \cdot \rho_w \frac{k_{\text{rel}} \boldsymbol{\kappa}}{\mu_w} \nabla p_w dx \\
& - \int_{\Omega} v_p \cdot \nabla \cdot \rho_w \frac{k_{\text{rel}} \boldsymbol{\kappa}}{\mu_w} \rho_w g e_z dx - \int_{\Omega} v_p \cdot Q_w dx + \int_{\Gamma_N} \bar{v}_p \cdot \left[\rho_w \frac{k_{\text{rel}} \boldsymbol{\kappa}}{\mu_w} \nabla^T p_w \cdot \mathbf{n} + g_N^{p_w} \right] d\sigma.
\end{aligned} \tag{1.24}$$

Since the \bar{v}_p and v_p are arbitrary test functions it is possible to set $\bar{v}_p = v_p$. This results in

$$\begin{aligned}
0 = & \int_{\Omega} v_p \cdot \phi \frac{\partial \rho_w}{\partial p} \frac{\partial p}{\partial t} S dx - \int_{\Omega} v_p \cdot \phi \rho_w \frac{\partial S}{\partial p_c} \frac{\partial p_c}{\partial t} dx \\
& + \int_{\Omega} \nabla^T v_p \cdot \rho_w \frac{k_{\text{rel}} \boldsymbol{\kappa}}{\mu_w} \nabla p_w dx \\
& - \int_{\Omega} v_p \cdot \nabla \cdot \rho_w \frac{k_{\text{rel}} \boldsymbol{\kappa}}{\mu_w} \rho_w g e_z dx - \int_{\Omega} v_p \cdot Q_w dx + \int_{\Gamma_N} v_p \cdot g_N^{p_w} d\sigma.
\end{aligned} \tag{1.25}$$

1.2.4 Finite Element Discretization

The pressure of the wet phase p_w is approximated by

$$p_w \approx \widetilde{p}_w = \sum N_j \widehat{p}_j = N \widehat{p}, \tag{1.26}$$

using the shape functions N_j and time dependent coefficients \widehat{p}_j . Using the shape functions again as test functions (Galerkin principle) the discretization of (1.25)) takes the following form

$$\begin{aligned}
0 = & \int_{\Omega} N \cdot \phi \frac{\partial \rho_w}{\partial p} \frac{\partial p}{\partial t} S dx - \int_{\Omega} N \cdot \phi \rho_w \frac{\partial S}{\partial p_c} \frac{\partial p_c}{\partial t} dx \\
& + \int_{\Omega} \nabla^T N \cdot \rho_w \frac{k_{\text{rel}} \boldsymbol{\kappa}}{\mu_w} \nabla N \widehat{p} dx \\
& - \int_{\Omega} N \cdot \nabla \cdot \rho_w \frac{k_{\text{rel}} \boldsymbol{\kappa}}{\mu_w} \rho_w g e_z dx - \int_{\Omega} N \cdot Q_w dx + \int_{\Gamma_N} N \cdot g_N^{p_w} d\sigma.
\end{aligned} \tag{1.27}$$

This is a set of equations of the form

$$\mathbf{M}_{pp} \widehat{p} + \mathbf{K}_{pp} \widehat{p} + \boldsymbol{\Psi}_p = 0 \tag{1.28}$$

with

$$\mathbf{M}_{pp} = \int_{\Omega} N \cdot \phi \frac{\partial \rho_w}{\partial p} \frac{\partial p}{\partial t} S dx - \int_{\Omega} N \cdot \phi \rho_w \frac{\partial S}{\partial p_c} \frac{\partial p_c}{\partial t} dx \tag{1.29}$$

$$\mathbf{K}_{pp} = \int_{\Omega} \nabla^T N \cdot \rho_w \frac{k_{\text{rel}} \boldsymbol{\kappa}}{\mu_w} \nabla N dx \tag{1.30}$$

$$\boldsymbol{\Psi}_p = - \int_{\Omega} N \cdot \nabla \cdot \rho_w \frac{k_{\text{rel}} \boldsymbol{\kappa}}{\mu_w} \rho_w g e_z dx - \int_{\Omega} N \cdot Q_w dx + \int_{\Gamma_N} N \cdot g_N^{p_w} d\sigma. \tag{1.31}$$

1.3 Mass Diffusion Equation

The primary variable in the mass diffusion process is the concentration C . In the general balance equation (1.5) the function $S(u(x, t))$ is substituted by $\phi R C$, where ϕ is the porosity and R denotes the retardation factor. The term J , describing the mass flow, is substituted by

$$qC - \mathbf{D} \text{grad} C, \tag{1.32}$$

i.e., there is advective and diffusive flow. The advective part qC is driven by the Darcy velocity q of the coupled groundwater flow. Finally, the term

$$\phi R \vartheta C \quad (1.33)$$

describing the decay of the chemical species is integrated into the equation which acts similarly to a sink term. Here ϑ is the decay rate. The balance equation reads:

$$\frac{\partial}{\partial t} (\phi RC) + \operatorname{div} (qC - \mathbf{D} \operatorname{grad} C) + \phi R \vartheta C - Q_C = 0 \quad (1.34)$$

where

- \mathbf{D} hydrodynamic dispersion tensor,

$$\mathbf{D} = (\phi D_d + \beta_T \|q\|) \mathbf{I} + (\beta_L - \beta_T) \frac{qq^T}{\|q\|}$$

where

- β_L is the longitudinal dispersivity of chemical species
- β_T is the transverse dispersivity of chemical species
- D_d is the molecular diffusion coefficient

- ϑ is the decay rate

Incompressible solid, i.e. $\frac{\partial \phi}{\partial t} = 0$, and the retardation factor is not time dependent:

$$\phi R \frac{\partial C}{\partial t} + \operatorname{div} (qC - \mathbf{D} \operatorname{grad} C) + \phi R \vartheta C - Q_C = 0 \quad (1.35)$$

1.3.1 Boundary Conditions

$$C = g_D^C \quad \text{on} \quad \Gamma_D \quad (\text{Dirichlet type boundary conditions}) \quad (1.36)$$

$$-\langle \mathbf{D} \operatorname{grad} C | n \rangle = g_N^C \quad \text{on} \quad \Gamma_N \quad (\text{Neumann type boundary conditions}) \quad (1.37)$$

1.3.2 Weak Formulation

The integration of the reformulated Neumann type boundary condition, i.e., $\langle \mathbf{D} \operatorname{grad} C | n \rangle + g_N^C = 0$, into (1.35), multiplying with arbitrary test functions $v, \bar{v} \in H_0^1(\Omega)$ and integration over Ω results in

$$\begin{aligned} 0 = & \int_{\Omega} v \cdot \phi \cdot R \cdot \frac{\partial C}{\partial t} d\Omega + \int_{\Omega} v \cdot \operatorname{div} (qC - \mathbf{D} \operatorname{grad} C) d\Omega \\ & + \int_{\Omega} v \cdot [\vartheta \cdot \phi \cdot R \cdot C] d\Omega - \int_{\Omega} v \cdot Q_C d\Omega + \int_{\Gamma_N} \bar{v} \cdot [\langle \mathbf{D} \operatorname{grad} C | n \rangle + g_N^C] d\sigma \end{aligned} \quad (1.38)$$

Integration by parts of the second term in the above equation yields:

$$\int_{\Omega} v \cdot \operatorname{div} (qC - \mathbf{D} \operatorname{grad} C) d\Omega = - \int_{\Omega} \langle \operatorname{grad} v | qC - \mathbf{D} \operatorname{grad} C \rangle d\Omega + \int_{\Omega} \operatorname{div} [v (qC - \mathbf{D} \operatorname{grad} C)] d\Omega \quad (1.39)$$

Using Green's formula for the last term of the above expression

$$\begin{aligned} \int_{\Omega} \operatorname{div} [v (qC - \mathbf{D} \operatorname{grad} C)] \, d\Omega &= \oint_{\Gamma} \langle v (qC - \mathbf{D} \operatorname{grad} C) | n \rangle \, d\sigma \\ &= \int_{\Gamma_D} \langle v (qC - \mathbf{D} \operatorname{grad} C) | n \rangle \, d\sigma + \int_{\Gamma_N} \langle v (qC - \mathbf{D} \operatorname{grad} C) | n \rangle \, d\sigma \end{aligned}$$

and since v vanishes on Γ_D the integral over Γ_D also vanishes, this leads to

$$\int_{\Omega} v \cdot \operatorname{div} (qC - \mathbf{D} \operatorname{grad} C) \, d\Omega = - \int_{\Omega} \langle \operatorname{grad} v | qC - \mathbf{D} \operatorname{grad} C \rangle \, d\Omega + \int_{\Gamma_N} \langle v (qC - \mathbf{D} \operatorname{grad} C) | n \rangle \, d\sigma \quad (1.40)$$

Thus (1.38) reads:

$$\begin{aligned} 0 &= \int_{\Omega} v \cdot \phi \cdot R \cdot \frac{\partial C}{\partial t} \, d\Omega - \int_{\Omega} \langle \operatorname{grad} v | qC - \mathbf{D} \operatorname{grad} C \rangle \, d\Omega + \int_{\Gamma_N} \langle v (qC - \mathbf{D} \operatorname{grad} C) | n \rangle \, d\sigma \\ &\quad + \int_{\Omega} v \cdot [\vartheta \cdot \phi \cdot R \cdot C] \, d\Omega - \int_{\Omega} v \cdot Q_C \, d\Omega + \int_{\Gamma_N} \bar{v} \cdot [\langle \mathbf{D} \operatorname{grad} C | n \rangle + g_N^C] \, d\sigma \end{aligned} \quad (1.41)$$

Setting $v = \bar{v}$:

$$\begin{aligned} 0 &= \int_{\Omega} \bar{v} \cdot \phi \cdot R \cdot \frac{\partial C}{\partial t} \, d\Omega - \int_{\Omega} \langle \operatorname{grad} \bar{v} | qC - \mathbf{D} \operatorname{grad} C \rangle \, d\Omega + \int_{\Gamma_N} \langle \bar{v} qC | n \rangle \, d\sigma \\ &\quad + \int_{\Omega} \bar{v} \cdot [\vartheta \cdot \phi \cdot R \cdot C] \, d\Omega - \int_{\Omega} \bar{v} \cdot Q_C \, d\Omega + \int_{\Gamma_N} \bar{v} \cdot g_N^C \, d\sigma \end{aligned} \quad (1.42)$$

1.3.3 Finite Element Discretization

The concentration is approximated by:

$$C \approx \sum N_j^C c_j = N^C c \quad (1.43)$$

using the shape functions N_j^C and time dependent coefficients c_j . Using the shape functions again as test functions (Galerkin principle) the discretization of (1.42)) takes the following form

$$\begin{aligned} 0 &= \int_{\Omega} N_i^C \cdot \phi \cdot R \cdot N_j^C \frac{\partial c_j}{\partial t} \, d\Omega - \int_{\Omega} \nabla^T N_i^C \cdot q \cdot N_j^C c_j \, d\Omega + \int_{\Omega} \nabla^T N_i^C \mathbf{D} \nabla N_j^C c_j \, d\Omega + \int_{\Gamma_N} (N_i^C q^T N_j^C c_j) n \, d\sigma \\ &\quad + \int_{\Omega} N_i^C \cdot [\vartheta \cdot \phi \cdot R \cdot N_j^C c_j] \, d\Omega - \int_{\Omega} N_i^C \cdot Q_C \, d\Omega + \int_{\Gamma_N} N_i^C \cdot g_N^C \, d\sigma \end{aligned} \quad (1.44)$$

This is a set of equations of the form

$$\mathbf{C}^{CC} \dot{c} + \mathbf{K}^{CC} c + f^C = 0 \quad (1.45)$$

with

$$\begin{aligned} \mathbf{K}_{ij}^{CC} &= - \int_{\Omega} \nabla^T N_i^C \cdot q \cdot N_j^C \, d\Omega + \int_{\Omega} \nabla^T N_i^C \mathbf{D} \nabla N_j^C \, d\Omega + \int_{\Gamma_N} (N_i^C \cdot q^T N_j^C)^T n \, d\sigma \\ &\quad + \int_{\Omega} N_i^C \cdot [\vartheta \cdot \phi \cdot R \cdot N_j^C] \, d\Omega, \end{aligned} \quad (1.46)$$

$$f_i^C = - \int_{\Omega} N_i^C Q_C \, d\Omega + \int_{\Gamma_N} N_i^C g_N^C \, d\sigma, \quad (1.47)$$

$$\mathbf{C}_{ij}^{CC} = \int_{\Omega} N_i^C \cdot \phi \cdot R \cdot N_j^C \, d\Omega. \quad (1.48)$$

In (1.46) the Darcy velocity q is assumed to be known from the hydrological process. In contrast to this approach pressure p in the Darcy velocity can be expressed as an approximation by shape functions N_i^p

$$q = \frac{\kappa}{\mu} \mathbf{grad}(p + \varrho \cdot g \cdot z) \approx \frac{\kappa}{\mu} (\nabla N_i^p + \varrho \cdot g \cdot e_z). \quad (1.49)$$

Thus, some terms of \mathbf{K}_{ij}^{CC} are moved to the coupling matrix:

$$\mathbf{K}_{ij}^{Cp} = - \int_{\Omega} \nabla^T N_i^C \cdot \frac{\kappa}{\mu} (\nabla N_i^p + \varrho \cdot g \cdot e_z) \cdot N_j^C d\Omega \quad (1.50)$$

1.4 Evaluating Dominance of Effects

Substitute variables and coefficients that appear in (1.35):

see 7.7 in [2]

$$\phi R \frac{\partial C}{\partial t} = \phi^* \phi_c R^* R_c \left(\frac{\partial C}{\partial t} \right)^* \left(\frac{\partial C}{\partial t} \right)_c = \phi^* \phi_c R^* R_c \left(\frac{\partial C}{\partial t} \right)^* \frac{(\Delta C)_c}{(\Delta t)_c} = \phi^* R^* \left(\frac{\partial C}{\partial t} \right)^* \phi_c R_c \frac{(\Delta C)_c}{t_c} \quad (1.51)$$

where $t_c = (\Delta t)_c$.

$$\begin{aligned} \operatorname{div}(qC) &= \frac{\partial qC}{\partial x_i} = \frac{\partial q}{\partial x_i} C + \frac{\partial C}{\partial x_i} q = \left(\frac{\partial q}{\partial x_i} \right)^* \frac{(\Delta q)_c}{L_c^{(q)}} C^* C_c + \left(\frac{\partial C}{\partial x_i} \right)^* \frac{(\Delta C)_c}{L_c^{(C)}} q^* q_c \\ &= \frac{\partial q^*}{\partial x_i^*} C^* \frac{(\Delta q)_c}{L_c^{(q)}} C_c + q^* \frac{\partial C^*}{\partial x_i^*} \frac{q_c (\Delta C)_c}{L_c^{(C)}} \end{aligned} \quad (1.52)$$

$$\begin{aligned} \operatorname{div}(\mathbf{D} \mathbf{grad} C) &= \frac{\partial}{\partial x_i} \left(\mathbf{D} \frac{\partial C}{\partial x_i} \right) = \left(\frac{\partial}{\partial x_i} \right)^* \frac{1}{L_c^{(C)}} \left(\mathbf{D}^* D_c \left(\frac{\partial C}{\partial x_i} \right)^* \frac{(\Delta C)_c}{L_c^{(C)}} \right) \\ &= \frac{\partial}{\partial x_i^*} \left(\mathbf{D}^* \frac{\partial C^*}{\partial x_i^*} \right) \frac{D_c (\Delta C)_c}{L_c^{(C)2}} \end{aligned} \quad (1.53)$$

$$\phi R \vartheta C = \phi^* \phi_c R^* R_c \vartheta^* \vartheta_c C^* C_c = \phi^* R^* \vartheta^* C^* \phi_c R_c \vartheta_c C_c \quad (1.54)$$

With $L_c^{(C)} = L_c^{(q)} = L_c$

$$\begin{aligned} 0 &= \phi^* R^* \left(\frac{\partial C}{\partial t} \right)^* \phi_c R_c \frac{(\Delta C)_c}{t_c} + \frac{(\Delta q)_c}{L_c} C_c \frac{\partial q^*}{\partial x_i^*} C^* + \frac{q_c (\Delta C)_c}{L_c} q^* \frac{\partial C^*}{\partial x_i^*} - \frac{D_c (\Delta C)_c}{L_c^2} \frac{\partial}{\partial x_i^*} \left(\mathbf{D}^* \frac{\partial C^*}{\partial x_i^*} \right) \\ &\quad + \phi_c R_c \vartheta_c C_c \phi^* R^* \vartheta^* C^* \end{aligned} \quad (1.55)$$

$$\begin{aligned} 0 &= \phi^* R^* \left(\frac{\partial C}{\partial t} \right)^* + \frac{1}{\phi_c R_c} \left(\frac{(\Delta q)_c}{(\Delta C)_c} C_c \frac{t_c}{L_c} \frac{\partial q^*}{\partial x_i^*} C^* + q_c \frac{t_c}{L_c} q^* \frac{\partial C^*}{\partial x_i^*} - D_c \frac{t_c}{L_c^2} \frac{\partial}{\partial x_i^*} \left(\mathbf{D}^* \frac{\partial C^*}{\partial x_i^*} \right) \right) \\ &\quad + \frac{\vartheta_c C_c t_c}{(\Delta C)_c} \phi^* R^* \vartheta^* C^* \end{aligned} \quad (1.56)$$

$$\begin{aligned} 0 &= \phi^* R^* \left(\frac{\partial C}{\partial t} \right)^* + \frac{D_c t_c}{\phi_c R_c L_c^2} \left(\frac{(\Delta q)_c}{(\Delta C)_c} C_c \frac{L_c}{D_c} \frac{\partial q^*}{\partial x_i^*} C^* + q_c \frac{L_c}{D_c} q^* \frac{\partial C^*}{\partial x_i^*} - \frac{\partial}{\partial x_i^*} \left(\mathbf{D}^* \frac{\partial C^*}{\partial x_i^*} \right) \right) \\ &\quad + \frac{\vartheta_c C_c t_c}{(\Delta C)_c} \phi^* R^* \vartheta^* C^* \end{aligned} \quad (1.57)$$

With $C_c = (\Delta C)_c$ and $q_c = (\Delta q)_c$

$$0 = \phi^* R^* \left(\frac{\partial C}{\partial t} \right)^* + \frac{D_c t_c}{\phi_c R_c L_c^2} \left(q_c \frac{L_c}{D_c} \frac{\partial q^*}{\partial x_i^*} C^* + q_c \frac{L_c}{D_c} q^* \frac{\partial C^*}{\partial x_i^*} - \frac{\partial}{\partial x_i^*} \left(\mathbf{D}^* \frac{\partial C^*}{\partial x_i^*} \right) \right) + \vartheta_c t_c \phi^* R^* \vartheta^* C^* \quad (1.58)$$

$$0 = \phi^* R^* \left(\frac{\partial C}{\partial t} \right)^* + \frac{D_c t_c}{\phi_c R_c L_c^2} \left(q_c \frac{L_c}{D_c} \frac{\partial q^* C^*}{\partial x_i^*} - \frac{\partial}{\partial x_i^*} \left(\mathbf{D}^* \frac{\partial C^*}{\partial x_i^*} \right) \right) + \vartheta_c t_c \phi^* R^* \vartheta^* C^* \quad (1.59)$$

Setting $Pe = q_c \frac{L_c}{D_c}$, the Peclet number and $Fo = q_c \frac{t_c D_c}{L_c^2}$ the Fourier number

$$0 = \phi^* R^* \left(\frac{\partial C}{\partial t} \right)^* + \frac{Fo}{\phi_c R_c} \frac{\partial}{\partial x_i^*} \left(Pe \cdot q^* C^* - \left(\mathbf{D}^* \frac{\partial C^*}{\partial x_i^*} \right) \right) + \vartheta_c t_c \phi^* R^* \vartheta^* C^* \quad (1.60)$$

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