

OpenGeoSys 6: Implementation of the *HT* Process

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1 *HT* process

The hydro-thermal (*HT*) process in porous media consists of the coupling of groundwater and thermal flow processes. Both processes are described using partial differential equations (pde) of parabolic type.

Sec. 1.1 is a general motivation to parabolic pde's which is very similar to [1].

Further reading: [4] [5] [2] [3]

1.1 Balance Equations

Let Ω be a domain, Γ the boundary of the domain and let u be an intrinsic quantity (for instance mass or heat) and the volume density is described by a function $S(u)$. The amount of the quantity in the domain can vary within time by two reasons. Firstly, new quantity can accumulate by flow over Γ or secondly it can be generated due to the presence of sources or sinks within Ω . Consequently, the balance reads

$$(1.1) \quad \frac{\partial}{\partial t} \int_{\Omega} S(u(x, t)) dx = - \int_{\Gamma} \langle J(x, t) | n(x) \rangle d\sigma + \int_{\Omega} Q(x, t) dx,$$

where $J(x, t)$ is the flow over the boundary, n is normal vector pointing outside of Ω , $d\sigma$ is an infinitesimal small surface element and $Q(x, t)$ describes sources and sinks within Ω . Further mathematical manipulations leads to

$$(1.2) \quad \int_{\Omega} \frac{\partial S(u(x, t))}{\partial t} dx + \int_{\Gamma} \langle J(x, t) | n(x) \rangle d\sigma - \int_{\Omega} Q(x, t) dx = 0.$$

Applying the theorem of Gauss yields to

$$(1.3) \quad \int_{\Omega} \frac{\partial S(u(x, t))}{\partial t} dx + \int_{\Omega} \operatorname{div} J(x, t) dx - \int_{\Omega} Q(x, t) dx = 0.$$

Finally,

$$(1.4) \quad \int_{\Omega} \left[\frac{\partial S(u(x, t))}{\partial t} + \operatorname{div} J(x, t) - Q(x, t) \right] dx = 0.$$

Since the domain is arbitrary it holds:

$$(1.5) \quad \frac{\partial S(u(x, t))}{\partial t} + \operatorname{div} J(x, t) - Q(x, t) = 0.$$

Depending on the constitutive law that describes the flow J , we obtain the balance equation of the considered process. Important practical laws are

$$(1.6) \quad J^{(1)} = -\mathbf{K} \mathbf{grad} u = -\mathbf{K} \nabla u$$

which describes diffusive flow and

$$(1.7) \quad J^{(2)} = cu \quad (\text{where } c \text{ is a velocity vector})$$

which describes advective flow or a combination of (1.6) and (1.7). For instance, substituting (1.6) in (1.5) leads to the following parabolic partial differential equation:

$$(1.8) \quad \frac{\partial S(u(x, t))}{\partial t} - \nabla \cdot [\mathbf{K}(x, t) \nabla u(x, t)] - Q(x, t) = 0,$$

while the description of the flow by a combination of (1.6) and (1.7) yields to

$$(1.9) \quad \frac{\partial S(u(x, t))}{\partial t} - \nabla \cdot [\mathbf{K}(x, t) \nabla u(x, t) - cu(x, t)] - Q(x, t) = 0.$$

1.2 Groundwater Flow

1.2.1 Constitutive Law: Darcy Flow

In the modeling of groundwater flow we assume the validity of the Darcy law:

$$(1.10) \quad q = -\frac{\kappa}{\mu(T)} (\mathbf{grad} p + \varrho_f(T) \cdot g \cdot e_z) = -\frac{\kappa}{\mu(T)} \left(\mathbf{grad} \left(\underbrace{p + \varrho_f(T) \cdot g \cdot z}_{\Psi} \right) \right) = -\frac{\kappa}{\mu(T)} \mathbf{grad} \Psi$$

where

- T is the temperature in $[\Theta]$
- $q(x, t, T)$ is the Darcy velocity in $[\frac{L}{T}]$
- $p(x, t)$ is the pressure $[\frac{ML}{T^2} \frac{1}{L^2}]$,
- κ is the anisotropic intrinsic permeability tensor of the porous medium (that can depend on the saturation S $[L^2]$ which will lead to Richards flow)
- $\mu(T, p)$ is the temperature and pressure dependent dynamic viscosity $[\frac{ML}{T^2} \cdot T]$,
- $\varrho_f(x, t, T, p)$ is the temperature and pressure dependent mass density of the fluid $[\frac{M}{L^3}]$,
- g the gravitation constant $[\frac{L}{T^2}]$

1.2.2 Balance Equation

In the groundwater flow the function S in the balance equations (1.8) or (1.9) is replaced by $\phi\rho(x, t, p)$:

$$(1.11) \quad \frac{\partial \phi\rho(p, T)}{\partial t} - \text{div} \frac{\kappa}{\mu(T)} \mathbf{grad} \Psi - Q(x, t) = 0$$

where

- ϕ is the porosity of the solid
- $Q(x, t)$ describes the inner sources or sinks, in coupled processes sources and sinks Q can also result from changes of the other primary variable, for instance through the changing of temperature sources and sinks can arise

For the implementation it is assumed that the medium is incompressible, i.e., the porosity does not change and thus $\frac{\partial \phi}{\partial t} = 0$. So the first term of (1.12) is

$$\frac{\partial \phi \rho(p, T)}{\partial t} = \underbrace{\frac{\partial \phi}{\partial t}}_{=0} \rho(p, T) + \phi \frac{\partial \rho(p, T)}{\partial t} = \phi \left(\frac{\partial \rho}{\partial p} \frac{\partial p}{\partial t} + \frac{\partial \rho}{\partial T} \frac{\partial T}{\partial t} \right)$$

As a part of the Boussinesq approximation it is assumed that the last term of the above equation $\frac{\partial \rho}{\partial T} \frac{\partial T}{\partial t}$ vanishes. Furthermore, it is assumed that the density depends linearly on the pressure, i.e. $\frac{\partial \rho}{\partial p}$ is constant. Under this assumptions it is possible to summarize the (constant) porosity and the constant derivation $\frac{\partial \rho}{\partial p}$ into a new constant S and (1.11) changes to

$$(1.12) \quad S \frac{\partial p}{\partial t} - \operatorname{div} \left[\frac{\kappa}{\mu(T)} \mathbf{grad} \Psi \right] - Q(x, t) = 0$$

1.2.3 Boundary Conditions

$$(1.13) \quad p - g_{D,p} = 0 \quad \text{on} \quad \Gamma_D \quad (\text{Dirichlet type boundary conditions})$$

$$(1.14) \quad \left\langle \frac{\kappa}{\mu(T)} \mathbf{grad} \Psi | n \right\rangle + g_N = 0 \quad \text{on} \quad \Gamma_N \quad (\text{Neumann type boundary conditions})$$

1.2.4 Weak Formulation

Multiplying (1.12) with -1 and summing up with (1.14) leads to

$$(1.15) \quad -S \frac{\partial p}{\partial t} + \operatorname{div} \left[\frac{\kappa}{\mu(T)} \mathbf{grad} \Psi \right] + Q(x, t) + \left\langle \frac{\kappa}{\mu(T)} \mathbf{grad} \Psi | n \right\rangle + g_N = 0.$$

Since (1.15) holds true for arbitrary points of the domain, the equation stays valid if it is multiplied by test functions $v, \bar{v} \in H_0^1(\Omega)$ and the integration over the domain Ω and the Neumann boundary $\Gamma_{N,p}$, respectively:

$$(1.16) \quad \int_{\Omega} v \left(-S \frac{\partial p}{\partial t} + \operatorname{div} \left[\frac{\kappa}{\mu(T)} \mathbf{grad} \Psi \right] + Q(x, t) \right) dx + \int_{\Gamma_N} \bar{v} \left(\left\langle \frac{\kappa}{\mu(T)} \mathbf{grad} \Psi | n \right\rangle + g_N \right) d\sigma = 0$$

or equivalently

$$(1.17) \quad -\int_{\Omega} v S \frac{\partial p}{\partial t} dx + \int_{\Omega} v \left(\operatorname{div} \left[\frac{\kappa}{\mu(T)} \mathbf{grad} \Psi \right] \right) dx + \int_{\Omega} v Q(x, t) dx + \int_{\Gamma_N} \bar{v} \left\langle \frac{\kappa}{\mu(T)} \mathbf{grad} \Psi | n \right\rangle d\sigma + \int_{\Gamma_N} \bar{v} g_N d\sigma = 0$$

Integration by parts of the second term of (1.17) results in

$$(1.18) \quad \int_{\Omega} v \left(\operatorname{div} \left[\frac{\kappa}{\mu(T)} \mathbf{grad} \Psi \right] \right) dx = - \int_{\Omega} \left\langle \mathbf{grad} v | \frac{\kappa}{\mu(T)} \mathbf{grad} \Psi \right\rangle dx + \int_{\Omega} \operatorname{div} \left(v \left[\frac{\kappa}{\mu(T)} \mathbf{grad} \Psi \right] \right) dx$$

Using Green's formula for the last term of the above expression

$$(1.19) \quad \begin{aligned} \int_{\Omega} \operatorname{div} \left(v \left[\frac{\kappa}{\mu(T)} \mathbf{grad} \Psi \right] \right) dx &= \oint_{\Gamma} \left\langle v \frac{\kappa}{\mu(T)} \mathbf{grad} \Psi | n \right\rangle d\sigma \\ &= \int_{\Gamma_D} \left\langle v \frac{\kappa}{\mu(T)} \mathbf{grad} \Psi | n \right\rangle d\sigma + \int_{\Gamma_N} \left\langle v \frac{\kappa}{\mu(T)} \mathbf{grad} \Psi | n \right\rangle d\sigma \end{aligned}$$

and the integral on the Dirichlet boundary Γ_D vanishes because $v = 0$ holds. Finally, the expression (1.18) takes the form

$$(1.20) \quad \int_{\Omega} v \left[\operatorname{div} \left(\frac{\boldsymbol{\kappa}}{\mu(T)} \mathbf{grad} \Psi \right) \right] dx = - \int_{\Omega} \langle \mathbf{grad} v | \mathbf{K} \mathbf{grad} \Psi \rangle dx + \int_{\Gamma_N} \left\langle v \frac{\boldsymbol{\kappa}}{\mu(T)} \mathbf{grad} \Psi | n \right\rangle d\sigma$$

Putting (1.20) in (1.17) yields to

$$0 = - \int_{\Omega} v S \frac{\partial p}{\partial t} dx - \int_{\Omega} \left\langle \mathbf{grad} v | \frac{\boldsymbol{\kappa}}{\mu(T)} \mathbf{grad} \Psi \right\rangle dx + \int_{\Gamma_N} \left\langle v \frac{\boldsymbol{\kappa}}{\mu(T)} \mathbf{grad} \Psi | n \right\rangle d\sigma \\ + \int_{\Omega} v Q(x, t) dx + \int_{\Gamma_N} \bar{v} \left\langle \frac{\boldsymbol{\kappa}}{\mu(T)} \mathbf{grad} \Psi | n \right\rangle d\sigma + \int_{\Gamma_N} \bar{v} g_N d\sigma$$

Since the test functions are arbitrary, by setting $v = -\bar{v}$ the second and fourth term cancel each other. Multiplying by -1 results in

$$(1.21) \quad 0 = \int_{\Omega} v S \frac{\partial p}{\partial t} dx + \int_{\Omega} \left\langle \mathbf{grad} v | \frac{\boldsymbol{\kappa}}{\mu(T)} \mathbf{grad} \Psi \right\rangle dx - \int_{\Omega} v Q(x, t) dx - \int_{\Gamma_N} v g_N d\sigma.$$

1.2.5 Finite Element Discretization

$$(1.22) \quad p \approx \sum N_j a_j = Na, \quad \Psi \approx \sum N_j a_j + \varrho_f g z$$

where $N_i(x, y, z)$ are the *shape functions* and a_i are coefficients. Galerkin principle:

$$(1.23) \quad v = N_i$$

Substituting (1.22) and (1.23) in (1.21) leads to

$$(1.24) \quad \left[\int_{\Omega} N_i S N_j dx \right] \frac{\partial a_j}{\partial t} + \left[\int_{\Omega} \nabla^T N_i \frac{\boldsymbol{\kappa}}{\mu(T)} \nabla N_j dx \right] a + \int_{\Omega} \nabla^T N_i \frac{\boldsymbol{\kappa} \varrho_f g}{\mu(T)} e_z dx - \int_{\Omega} N_i Q(x, t) dx - \int_{\Gamma_N} N_i g_N d\sigma = 0,$$

$i, j = 1, \dots, n$, which is a set of linear equations of the form

$$(1.25) \quad \mathbf{C} \dot{a} + \mathbf{K} a + f = 0$$

with

$$(1.26) \quad \mathbf{C}_{ij} = \int_{\Omega} N_i S N_j dx$$

$$(1.27) \quad \mathbf{K}_{ij} = \int_{\Omega} \nabla^T N_i \frac{\boldsymbol{\kappa}}{\mu(T)} \nabla N_j dx$$

$$(1.28) \quad f_i = - \int_{\Omega} N_i Q(x, t) dx - \int_{\Gamma_N} N_i g_N d\sigma + \int_{\Omega} \nabla^T N_i \frac{\boldsymbol{\kappa} \varrho_f g}{\mu(T)} e_z dx$$

1.3 Heat Conduction Equation

1.3.1 Fick's Law

$$(1.29) \quad J = -\lambda \mathbf{grad} T$$

where T is the temperature, λ is the hydrodynamic thermodispersion tensor and J the heat flow

1.3.2 Balance Equation

The heat conduction equation is also known as the advection-diffusion or convection-diffusion equation.

$$(1.30) \quad \underbrace{[\varrho_f(x)\phi c_f + \varrho_s(x)(1-\phi)c_s]}_{:=c_p} \cdot \frac{\partial T}{\partial t} - \operatorname{div}(\lambda \mathbf{grad} T) + \varrho_f \cdot c_f(x) \cdot \langle q | \mathbf{grad} T \rangle = 0$$

where

- q is the Darcy velocity defined by (1.10)
- ϱ_s is the solid density $[\frac{M}{L^3}]$
- λ hydrodynamic thermodispersion tensor,

$$\lambda = \lambda^{\text{cond}} + \lambda^{\text{disp}}$$

- $\lambda^{\text{cond}}(\phi) = \phi\lambda_f + (1-\phi)\lambda_s$ is the thermal conductivity
- $\lambda^{\text{disp}}(\alpha_T, \alpha_L) = \varrho_f c_f \left[\alpha_T \|q\|_2 \mathbf{I} + (\alpha_L - \alpha_T) \frac{qq^T}{\|q\|_2} \right]$ is the thermal dispersivity, where α_T is the transverse thermodispersivity and α_L is the longitudinal thermodispersivity of the fluid
- ϕ is the porosity

1.3.3 Boundary Conditions

$$(1.31) \quad T = g_D^T \quad \text{on} \quad \Gamma_D \quad (\text{Dirichlet type boundary conditions})$$

$$(1.32) \quad -\langle \lambda \mathbf{grad} T | n \rangle = g_N^T \quad \text{on} \quad \Gamma_N \quad (\text{Neumann type boundary conditions})$$

1.3.4 Weak Formulation

The integration of the reformulated Neumann type boundary condition, i.e., $\langle \lambda \mathbf{grad} T | n \rangle + g_N^T = 0$, into (1.30), multiplying with arbitrary test functions $v, \bar{v} \in H_0^1(\Omega)$ and integration over Ω results in

$$(1.33) \quad - \int_{\Omega} v \cdot \operatorname{div}(\lambda \mathbf{grad} T) \, d\Omega + \int_{\Omega} v \cdot \varrho_f \cdot c_f(x) \langle q | \mathbf{grad} T \rangle \, d\Omega + \int_{\Omega} v \cdot c_p(x) \cdot \frac{\partial T}{\partial t} \, d\Omega + \int_{\Gamma_N} \bar{v} \cdot [\langle \lambda \mathbf{grad} T | n \rangle + g_N^T] \, d\sigma = 0$$

Integration by parts of the first term in the above equation yields:

$$(1.34) \quad \int_{\Omega} v \operatorname{div}[\lambda \mathbf{grad} T] \, d\Omega = - \int_{\Omega} \langle \mathbf{grad} v | [\lambda \mathbf{grad} T] \rangle \, d\Omega + \int_{\Omega} \operatorname{div}[v \lambda \mathbf{grad} T] \, d\Omega$$

Using Green's formulae for the last term of the above expression

$$(1.35) \quad \int_{\Omega} \operatorname{div}[v \lambda \mathbf{grad} T] \, d\Omega = \oint_{\Gamma} \langle v \lambda \mathbf{grad} T | n \rangle \, d\sigma = \int_{\Gamma_D} \langle v \lambda \mathbf{grad} T | n \rangle \, d\sigma + \int_{\Gamma_N} \langle v \lambda \mathbf{grad} T | n \rangle \, d\sigma$$

and since v vanishes on Γ_D the integral over Γ_D also vanishes, this leads to

$$(1.36) \quad \int_{\Omega} v [\operatorname{div}(\lambda \mathbf{grad} T)] \, d\Omega = - \int_{\Omega} \langle \mathbf{grad} v | \lambda \mathbf{grad} T \rangle \, d\Omega + \int_{\Gamma_N} \langle v \lambda \mathbf{grad} T | n \rangle \, d\sigma$$

Thus (1.33) reads:

$$(1.37) \quad 0 = - \int_{\Omega} \langle \mathbf{grad} v | \lambda \mathbf{grad} T \rangle d\Omega + \int_{\Gamma_N} \langle v \lambda \mathbf{grad} T | n \rangle d\sigma + \int_{\Omega} v \cdot \varrho_f \cdot c_f(x) \langle q | \mathbf{grad} T \rangle d\Omega \\ + \int_{\Omega} v \cdot c_p(x) \cdot \frac{\partial T}{\partial t} d\Omega + \int_{\Gamma_N} \bar{v} \cdot \langle \lambda \mathbf{grad} T | n \rangle d\sigma + \int_{\Gamma_N} \bar{v} \cdot g_N^T d\sigma$$

Setting $v = -\bar{v}$ and multiplying by -1 :

$$(1.38) \quad \int_{\Omega} \langle \mathbf{grad} v | \lambda \mathbf{grad} T \rangle d\Omega - \int_{\Omega} v \cdot \varrho_f \cdot c_f(x) \langle q | \mathbf{grad} T \rangle d\Omega - \int_{\Omega} v \cdot c_p(x) \cdot \frac{\partial T}{\partial t} d\Omega + \int_{\Gamma_N} v \cdot g_N^T d\sigma = 0$$

1.3.5 Finite Element Discretization

Analogously to the approximation (1.22) the temperature is approximated by:

$$(1.39) \quad T \approx \sum N_i b_i = N b$$

using the same shape functions N_i and time dependent coefficients b_i . Using the shape functions again as test functions (Galerkin principle (1.23)) the discretization of (1.38) takes the following form

$$(1.40) \quad 0 = \left[\int_{\Omega} \nabla^T N_i \lambda \nabla N d\Omega - \int_{\Omega} N_i \cdot \varrho_f \cdot c_f(x) \cdot q^T \cdot \nabla N d\Omega \right] b \\ + \left[\int_{\Omega} N_i \cdot c_p(x) N d\Omega \right] \frac{db}{dt} + \int_{\Gamma_N} N_i g_N^T d\sigma \quad (i = 1, \dots, n).$$

This is again a set of equations of the form

$$(1.41) \quad \mathbf{C} \dot{b} + \mathbf{K} b + f = 0$$

with

$$(1.42) \quad \mathbf{K}_{ij} = \int_{\Omega} \nabla^T N_i \lambda \nabla N_j d\Omega - \int_{\Omega} N_i \varrho_f c_f \langle q | \nabla N_j \rangle d\Omega$$

$$(1.43) \quad f_i = - \int_{\Omega} N_i Q(x, t) d\Omega - \int_{\Gamma_N} N_i g_N^T d\sigma$$

$$(1.44) \quad \mathbf{C}_{ij} = \int_{\Omega} N_i c_p N_j d\Omega$$

1.4 Coupling the Processes

The heat conduction process is coupled with the confined groundwater flow process by the advective term in (1.30).

The fluid density ϱ_f as well as the viscosity μ used in (1.10) (and respectively (1.12)) are coupled to the heat conduction process by their temperature dependencies.

For the fluid density the following linear dependency

$$(1.45) \quad \varrho_f(T) = \varrho_{\text{ref}} (1 - \beta(x) (T - T_{\text{ref}}))$$

is implemented, where the fluid thermal expansion coefficient $\beta(x)$ [K^{-1}] depends on the medium and T_{ref} is the reference temperature.

The temperature dependency of the fluid viscosity is implemented by the function:

$$(1.46) \quad \mu(T) = \mu_0 e^{-\frac{T-T_c}{T_v}}.$$

There is not implemented any coupling by source and sink terms in OGS-6, i.e., the density changes due to temperature changes affects only the buoyancy term $\rho_f(T) \cdot g \cdot z$ in (1.10). The currently implemented coupling schema is referred to as the Boussinesq approximation.

These simplified EOS are those used in the large-scale benchmark allowing to apply linear stability analysis of HT problem [6].

The IAPWS EOS for fluid density and viscosity are also implemented into OGS.

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